

Date: 6th May 2025

LLFA Comments Response Technical Note – 3/21/2245/FUL – Land to the west of the A507 betweed Cottered and Cromer, Hertfordshire, SG9 9PU

This technical note has been prepared to provide additional information requested by the Hertfordshire County Council (HCC) acting as Lead Local Flood Authority (LLFA) in the objection letters dated 9th of January 2025 and subsequent letter dated 18th of February 2025 in regards to the installation and operation of a solar farm including co-located energy storage facilities, onsite substation, ancillary infrastructure and landscaping at Land to the West of the A507 Between Cottered and Cromer, Hertfordshire, SG9 9PU. The objections raised by the LLFA are summarised below. Copies of both letters are available in Annex A of this technical note.

This technical note should also be read in conjunction with the Flood Risk Assessment (FRA) and Sustainable Drainage Strategy document HLEF85532 v3, dated October 2024 and associated Appendices.

In the letter dated 18th of February, the LLFA has stated that whilst the submission of the appendices has removed some of their previous objections (January 2025), watercourse consent, infiltration testing, infiltration rate, simple index approach and resilience measures have not been updated in this revision. Therefore, the objections to these remain.

The LLFA object to this planning application in the absence of an acceptable Drainage Strategy relating to:

- The proposed SuDS are likely to increase the risk of flooding elsewhere.
- The development is not in accordance with NPPF, PPG or local policies.
 - o Policy WAT1 Flood Risk Management
 - o Policy WAT3 Water Quality and the Water Environment
 - Policy WAT5 Sustainable Drainage

To prevent flooding in accordance with National Planning Policy Framework paragraphs 181, 182 and 187 by ensuring the satisfactory management of local flood risk, surface water flow paths, storage and disposal of surface water from the site in a range of rainfall events and ensuring the SuDS proposed operates as designed for the lifetime of the development.

LLFA OBJECTIONS

• Demonstrate that any residual risk is managed with appropriate flood resistance and residual measures. Residual Risk needs to be further explored.

- Identification is required to those structures which require consent for works on an ordinary
 watercourse (from the LLFA), this extends to works required within 8m from the top of the bank (see
 HCC LLFA website). Confirmation is required as to whether any works will be undertaken on the
 watercourse.
- Evidence required on ground conditions / BRE365 or similar infiltration testing / dissolution potential / seasonally high groundwater levels. Infiltration testing has not been provided for viability. This should be provided.
- Surface Watercourse does it connect to the wider network and is there permission and there are agreed access locations for proposed outfalls with the riparian owner? There is no in-principle agreement for connection into the River Beane in the north.
- The application must provide water quality benefits. Appropriate water quality assessment is absent / incorrect. Simple Index Approach has not been provided.
- The most precautionary infiltration rate should be used in the design of the attenuation feature. The infiltration rate has been assumed as the 'best case scenario'. The worst-case scenario rate should be used.
- Layout and/or drainage layout drawings need to show all the drainage features (storage and conveyance), with labels the same as those in the submitted supporting calculations. Confirmation of any formal drainage on site is required in a drawing. Currently, it is unclear as to whether formal drainage will be used on site.
- Drawings of cross sections and long sections of all the network and structures such as ponds, basins and swales need to be supplied. Confirmation of any formal drainage on site is required in a drawing. Currently, it is unclear as to whether formal drainage will be used on site.
- A high-level assessment of how water quantity and water quality will be managed during the construction phase is required. Identifying high level assumptions such as need to discharge to a sewer or watercourse with appropriate pollution measures. A high-level assessment of water quality during construction is required.

RPS RESPONSE

Residual Risk

- Residual flood risk is managed through the implementation of resilience measures which prioritise rapid recovery and minimise damage to critical infrastructure in case of exceedance of flood flows. The FRA includes resistance and resilience measures and these are summarised below:
 - Solar panels are mounted on elevated structures that allow water to pass underneath without affecting the modules or their electrical connections.
 - All cabling will be installed above predicted flood levels, using elevated trays or poles where possible.
 - Key electrical equipment inside substations will be installed at heights above predicted flood levels.
- These measures, combined with routine inspections which will be detailed in the detailed maintenance plan at detail design stage, will enhance the resilience of solar farm infrastructure and sufficiently address residual flood risk.

Structures within 8m from watercourse

A crossing over the ordinary watercourse is proposed to be upgraded. A drawing which includes the
proposed works and the cross section is available in Annex B of this Technical Note. We understand
that a Flood Risk Activity Permit (FRAP) or Land Drainage Consent would be required. The necessary
permits would be applied for following planning approval and subject to consultation with the EA/LLFA
at detailed design stage.

Infiltration Testing / Ground Conditions & Infiltration Rate

- Infiltration testing has not been undertaken at planning application stage because the surface water drainage strategy has been conservatively designed using a worst-case infiltration rate, assuming minimal or no infiltration potential. This approach ensures that the proposed drainage system is robust and does not rely on infiltration for effective operation, thereby eliminating any risk of under-design due to overestimation of infiltration capacity. As such, the current design presents a precautionary worst-case scenario in line with industry best practice.
- The original FRA included a typo ('best case' scenario) while in the Causeway Calculations available as Appendix H it can be confirmed that an infiltration coefficient close to zero was used in the storage calculations. Calculations were re-run to include no outfall and these are available in Annex C of this Technical Note. These demonstrate that the proposed gravel sub-bases for the ancillary building will accommodate the increased volumes from the proposed hardstanding at the site.
- Undertaking infiltration testing at this stage would offer limited additional value, as the strategy assumes minimal/ no infiltration potential and therefore does not depend on infiltration performance to demonstrate feasibility or compliance with planning policy. Conversely, it demonstrates that a feasible strategy can be implemented which does not rely on infiltration.

Surface Watercourse Connection

• No formal connection is proposed to the surface watercourses on site.

Simple Index Approach

- Surface water run-off should be managed by SuDS that are designed to attenuate flows and to avoid water quality impacts downstream. To demonstrate that surface water arising from the development will be appropriately treated prior to discharge, the Simple Index Approach, as outlined within the SuDS Manual (CIRIA C753) has been followed.
- As stated in the SuDS Manual 2015 (C753), the risk posed by surface water runoff to the receiving environment is a function of:
 - the pollution hazard at a particular site (i.e. the pollutant source);
 - the effectiveness of SuDS treatment components in reducing levels of pollutants to environmentally acceptable levels, groundwater (i.e. the pollutant pathway);
 - the sensitivity of the receiving environment (i.e. the environmental receptor).
- The CIRIA SuDS Manual (2015) provides pollution hazard indices from an assortment of land uses and the pollution mitigation indices for a number of SuDS techniques. It is noted that the pollution hazard indices are not cumulative, and that the mitigation should be designed to the maximum pollutant use. Furthermore, it is not anticipated that there would be coarse sediments for removal at the site, therefore specific design for this purpose would not be required.
- The development is classified as sites with 'low' pollution hazard levels. The pollutant hazard indices for this type of development are outlined in the SuDS Manual (CIRIA C753) Table 26.2 and Table 1 below.

Table 1. Pollution Hazard and Mitigation Indices

Land Use / SuDS Feature	Total Suspended Solids (TSS)	Metals	Hydrocarbons	
	Proposed Lan	d Uses		
Other roofs (typically commercial / industrial roofs)	0.3	0.2	0.05	
Mitigation				
Gravel Subbase	0.4	0.4	0.4	

- As illustrated in the Table 1 above, the identified mitigation indices (The SuDS Manual, CIRIA C753, Table 26.3) of the proposed gravel subbase exceed the maximum anticipated pollutant hazard indices. This confirms that surface water arising from the ancillary infrastructure on site will receive an appropriate level of treatment in advance of discharge from the site following natural infiltration patterns.
- The only potential source of higher pollution within the site are the transformers at the Substation site. These will be bunded, with any potential contamination held within the bund. Water captured within the bund would be extracted via a suitable qualified contractor for appropriate disposal.

Conceptual Drainage Layout Drawing

No formal drainage is proposed for the solar farm panels elements of the proposed development. The drainage strategy is described in Section 10 of the FRA report. An illustrative drawing showing the proposed measures to address the increase of impermeable area due to installation of ancillary infrastructure is available in Annex D of this technical note.

Compared to agricultural use, a solar farm is likely to be inherently better for surface water drainage than a continuation of the existing use. If a solar farm proposal avoids the creation of new hardstanding, includes mitigation for ancillary infrastructure, and will not alter existing landforms (e.g. levelling or bunds), a solar farm will not change existing characteristics and should be a positive improvement even with no additional SuDS measures.

The primary reason for this is the significant advantage from full year-round organically managed vegetated ground cover on a solar farm compared with intensive arable uses. Research undertaken by Cook and McCuen (2013) found that provided full vegetation cover beneath the solar panels is maintained, the change in runoff characteristics from solar farm sites is likely to be insignificant and that ground cover has a much more important control over runoff.

A solar farm already includes designed-in surface water flood risk mitigation. This is something solar PV planning applications do not always effectively communicate. It can be helpful to clarify some of the ways that surface water flood risk is addressed without adding-in new features.

The "requirement" for SuDS on development is set out in Paragraph 182 of the NPPF (2024) which states: "182. Applications which could affect drainage on or around the site should incorporate sustainable drainage systems to control flow rates and reduce volumes of runoff, and which are proportionate to the nature and scale of the proposal. These should provide multifunctional benefits wherever possible, through facilitating improvements in water quality and biodiversity, as well as benefits for amenity. Sustainable drainage systems provided as part of proposals for major development should:

- a) take account of advice from the lead local flood authority;
- b) have appropriate proposed minimum operational standards; and
- c) have maintenance arrangements in place to ensure an acceptable standard of operation for the lifetime of the development."

The requirement for SuDS is a "should", not a "must". It is our view that the lack of risk at the site, coupled with the temporary nature of the development, and a requirement for full reinstatement of the land, makes a case that SuDS beyond the minimum would be inappropriate.

The solar farm is a temporary development. Because the land will be returned to full agricultural use after the expiration of the temporary solar farm consent, SuDS that would require new intrusive or otherwise unnatural elements (e.g. pipework or tanks) or land shaping (e.g. swales) should only be required as a last resort to enable easy restoration to existing agricultural use with minimal ground disturbance or disruption to new and improved ecological features.

One of the multifunctional environmental benefits of a solar farm is soil quality improvement from cessation of intensive arable use and organic management of the land. It is expected that soil health will be improved through increase in soil organic matter, increase in the diversity of soil flora, fauna and microbes, and improved soil structure. All of the elements of a solar farm can be removed very easily with minimal topsoil disturbance which should leave the improved and enriched soil as a benefit for the return to agricultural use. Significant

works to remove filter drains or level out swales that are not complimentary to a return to agriculture would undermine this benefit.

This could also lead to more problems elsewhere. Although a solar farm is a temporary consent that does not change the greenfield land classification, its 40-year lifetime is not short. Temporary land drainage measures that might unnaturally change the existing baseline could subsequently be relied on off-site as part of the wider ecosystem services network. When the solar farm is decommissioned and these are removed/reversed, there is a risk of adverse "downstream" impacts for those who have relied on the SuDS. Therefore, although SuDS are intended to contribute to flood risk resilience, the nature of a solar farm and its whole-life context needs to be carefully considered so that the sustainable development can be implemented in a sustainable manner and with an eye on the future restoration to existing conditions and the resumption of agricultural use.

The nature of the proposed development means that precipitation would be intercepted by between 25% to 40% of the surface of the site that is typically over-sailed by solar panels. A known concern is the risk of water "sheeting" off a solar array façade. As a result of the construction of the solar panels, some rainfall will be intercepted by the surface of the arrays before reaching ground level. Intercepted rainfall will either run down the face of the panels and drip onto the ground below or will be lost due to evaporation from the face of the panels. Without mitigation there is a risk of erosion of the ground on which rainwater drips. This could then result in the formation of rivulets which could increase the speed at which runoff discharges from the site.

However, the potential for erosion to occur as a result of the 'drip effect' is appropriately mitigated by features of the solar arrays themselves and appropriate seeded vegetation which will be provided below and between rows of the solar panels to act as a level spreader/energy dissipater to promote low erosivity sheet flow during operation of the solar farm. The vegetation will be managed organically and will either be mowed or used for light grazing. The grassland will not only grow between array gaps, it includes all ground under the arrays as well. This means that excluding the access tracks and ancillary infrastructure most of the site will be fully vegetated species rich pastoral grassland.

Without any additional development being required, the gaps between the arrays are natural filter strips (SuDS). The key takeaway is that the majority of the site has mitigation and SuDS inherently designed-in. The arrays are designed to avoid sheeting/pooling/erosion. Water drips off at multiple points onto vegetated ground below. In addition, there is significant space between rows (typically around 2-6m) to act as natural filter strips with vegetated ground that slows the movement of surface water.

In terms of inverters and ancillary infrastructure, due to the small size of the units, and the widespread nature of their locations across the development, it is impractical to connect them into a drainage scheme. The inclusion of the proposed gravel subbase is considered to be sufficient and it would have a betterment on existing soil porosity. Water runoff from these infrastructure will slowly drain into the underlying ground through infiltration.

During events exceeding the 1 in 100 + 40% climate change event, any resulting above-ground flooding would be temporary with shallow depths and would not affect the infrastructure on site or significantly increase flood risk to off-site locations, mimicking current site conditions.

The new infrastructure on a permeable gravel base will not change an underlying condition beyond the topsoil. What would otherwise be topsoil will be replaced by gravel, which has 30% more porosity and storage capacity than the existing topsoil would have. This means even if the gravel base is insufficient for storage and infiltration, the resulting conditions are no different than they would be on the as-is farmland, except that the extra storage capacity of the gravel base is a betterment compared to the topsoil in the event that underlying conditions are not supporting effective infiltration.

In terms of the substation compound, the sub-base depth will depend on the size of the building. In the calculations we have used the worst case scenario where the all substation compound will be impermeable and therefore would need a 550mm deep sub-base to attenuate the flows. In reality, the impermeable area associated to the substation will be much smaller than that therefore potentially reducing the sub-base depth to 300mm.

Additionally, due to the temporary nature of the development, it is considered impractical to route flows from the ancillary infrastructure through the field to the watercourse.

Cross Sections of SuDS structures

• Cross sections of the gravel sub-bases will be provided at detailed design stage. It is proposed that details such as cross sections are secured by condition at the detailed design stage, once planning permission has been granted. This approach allows for the refinement of the drainage design while ensuring sufficient storage on site.

Water Quality during Construction

- A construction environmental management plan and a construction surface water management plan will be prepared in conjunction with the appointed contractor. It will include evidence of adequate provision of surface water management, both in terms of runoff quantity (flow rates and volumes), as well as quality (pollution mitigation). It will include pollution prevention measures including responsibility, mitigation if required and monitoring & controls.
- It is therefore proposed that a construction surface water management plan is secured by a condition and carried out at the detailed design stage, once planning permission is granted.

Conclusion.

We trust that this information sufficiently addresses your information requirements for removing your objections to the proposed development of the planning application reference no. 3/24/2245/FUL, however should you require any further information or clarification then we would be happy to provide this.

Yours sincerely, for RPS Consulting Services Ltd

Francesca Caggiano Associate Consultant - Hydrology Francesca.caggiano@rpsgroup.com +44 02072803246

Annex A – LLFA Objections Letters

Growth & Environment



David Lamb East Herts District Council Wallfields Pegs Lane Hertford Hertfordshire HP1 1DN Lead Local Flood Authority Growth and Environment Hertfordshire County Council Post Point CHN 215 Farnham House Six Hills Way, Stevenage HERTFORDSHIRE, SG1 2ST www.hertfordshire.gov.uk

Contact: Flood Risk Management Team Email: <u>FRMConsultations@hertfordshire.gov.uk</u>

Date 18 February 2025

Dear David

RE: 3/24/2245/FUL – Installation and operation of a solar farm including co-located energy storage facilities, onsite substation, ancillary infrastructure and landscaping – Land to the West of the A507 Between Cottered and Cromer, Hertfordshire, SG9 9PU

Thank you for your re-consultation on the above site, received on 29 January 2025. We have reviewed the application as submitted and wish to make the following comments.

This is a Full Planning Application for a new solar farm including co-located energy storage facilities, onsite substation, ancillary infrastructure and landscaping.

We previously responded on the 9 January 2025 requesting the provision of the appendix and had several other objections to this proposal. Whilst the submission of the appendix has removed some of our previous objections, watercourse consent, infiltration testing, infiltration rate, simple index approach and resilience measures have not been updated in this revision. Therefore, the objections to these remain.

We **object** to this planning application in the absence of an acceptable Drainage Strategy relating to:

- The proposed SuDS are likely to increase the risk of flooding elsewhere.
- The development is not in accordance with NPPF, PPG or local policies.
 - Policy WAT1 Flood Risk Management
 - Policy WAT3 Water Quality and the Water Environment
 - Policy WAT5 Sustainable Drainage

Reason

To prevent flooding in accordance with National Planning Policy Framework paragraphs 181, 182 and 187 by ensuring the satisfactory management of local flood risk, surface

Creating a cleaner, greener, healthier Hertfordshire

water flow paths, storage and disposal of surface water from the site in a range of rainfall events and ensuring the SuDS proposed operates as designed for the lifetime of the development.

We will consider reviewing this objection if the issues highlighted on the accompanying Planning Application Technical Response document are adequately addressed.

Informative

For further advice on what we expect to be contained within the FRA and/ or a Drainage Strategy to support a planning application, please refer to the Validation List and Proforma on our surface water drainage webpage

https://www.hertfordshire.gov.uk/services/recycling-waste-and-

<u>environment/water/surface-water-drainage/surface-water-drainage.aspx</u> this link also includes HCC's Flood Risk Management policies on SuDS in Hertfordshire. We do expect the Validation List to be submitted to the Local Planning Authority and LLFA to show you have provided all information and the Proforma to the LLFA to summarise the details of the proposed development.

Erection of flow control structures or any culverting of an ordinary watercourse requires consent from the appropriate authority, which in this instance is Hertfordshire Lead Local Flood Authority and the Local Council (if they have specific land drainage bylaws). It is advised to discuss proposals for any works at an early stage of proposals.

Please note if, you the Local Planning Authority review the application and decide to grant planning permission, notify the us (the Lead Local Flood Authority), by email at <u>FRMConsultations@hertfordshire.gov.uk</u>.

Yours sincerely

Ellie

Ellie Miller SuDS and Watercourses Support Officer Growth and Environment

Annex

The following documents have been reviewed.

- Report: Flood Risk Assessment and Sustainable Drainage Strategy Appendix (A-I), prepared by RPS, October 2024, REF HILEF85532 REV 3
- Report: Flood Risk Assessment and Sustainable Drainage Strategy, prepared by RPS, October 2024, REF HILEF85532 REV 3
- Report: Flood Risk Sequential Test, prepared by RPS, November 2024, REF HILEF85532 REV 5

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordsh
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	



Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordshire
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

FULL APPLICATION	Related Policy or Standard	Applicant Action Required	LLFA Specific Comment
Long term sustainability of the development	NPPF Paragraph 176 and 181 PPG Paragraph 004, 036, 061, 068 and 069 Policy WAT1 Flood Risk Management	Provide site specific ordinary watercourse or surface water flow path hydrological and hydraulic modelling.	Not required – Surface Water modelling / Fluvial modelling has been undertaken.
		Demonstrate that any residual risk is managed with appropriate flood resistance and resilience measures.	Objection: Residual risk needs to be further explored.
How does the site currently drain?		⊠Include evidence of appropriate freeboard to finished floor levels from the design flood level.	Objection: Floor levels are contained in Appendix F which has not been provided. We cannot provide comment until this has been provided.
	NPPF Paragraph 182 PPG Paragraph 059 SDNSTS S1, S2, S3, S4, S5, S6 Policy WAT1 Flood Risk Management	□ Include appropriate climate change allowance on modelling scenarios for assessment of the lifetime of the development (including the 3.33% AEP design flood event).	Not required – Surface Water modelling / Fluvial modelling has been undertaken.
		□Use up to date FEH2013 or 2022 rainfall data for all design flood events.	Not required – Surface Water modelling / Fluvial modelling has been undertaken.
		☑ Identification is required of those structures which require consent for works on an ordinary watercourse (from the LLFA), this extends to works required within 8m from the top of the bank (see HCC LLFA website).	Objection: Confirmation is required as to whether any works will be undertaken on the watercourse.
		Evidence required on ground conditions / BRE365 or similar infiltration testing / dissolution potential / seasonally high groundwater levels.	Objection: Infiltration testing has not been provided for viability. This should be provided.
		Greenfield runoff rates and volumes are missing or need to be recalculated (incorrect input parameters).	Objection: Volumes have not been provided.
		Pre-development brownfield runoff rates are missing or need to be recalculated (incorrect input parameters).	Not required – Greenfield site.

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordshire
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

FULL APPLICATION	Related Policy or Standard	Applicant Action Required	LLFA Specific Comment
		□Drawing required to show where existing drainage network and outfall/s are, plus confirmation if will they be retained or removed.	Included – Field Drainage (informal).
		□ Drainage survey required to provide evidence of existing discharge rate and condition (may include detailed asset or CCTV survey and estimation of discharge from an existing pipe diameter/slope).	Not required – Only informal field drainage.
Where will the site drain to?	NPPF Paragraph 182 PPG Paragraph 055, 056, 059, 060, 061, 062 and 063 SDNSTS S12, 13 and S14 Policy WAT3 - Water Quality and the Water Environment	Drainage location hierarchy has not been followed, further information is required on;	Solar Farm – Not practical.
		 Evidence why rainwater reuse can't be included. 	
		Source control and interception has not been provided by the provision of vegetated SuDS.	Informative: Further consideration to vegetated SuDS.
		☑ Infiltration proposals – re Groundwater Source Protection Zone I restrictions (only clean roof water in a sealed system may be discharged).	Objection: Infiltration testing has not been provided for viability. This should be provided.
		Surface watercourse – does it connect to the wider network and is there permission and there are agreed access locations for proposed outfalls with the riparian owner?	Objection: There is no in- principle agreement for connection into the River Beane in the north.
		□Surface water sewer – no in principle agreement from owner of the asset.	Not required – Not proposed.
		□ Combined sewer – no in principle agreement from owner of the asset.	Not required – Not proposed.
		□ In principle objection - proposing to connect surface water runoff to foul sewer.	Not required – Not proposed.

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertford
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	



Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordshire
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

FULL APPLICATION	Related Policy or Standard	Applicant Action Required	LLFA Specific Comment
effecting flood risk elsewhere?	SDNSTS S2, S3, S4, S5, S6 Policy WAT5 Sustainable Drainage	☑ Infiltration rates are shown to be favourable and should be used in the drainage design (where appropriate).	Objection: The infiltration rate has been assumed as the 'best case scenario'. The worst-case scenario rate should be used.
		☑ Infiltration storage drainage design should be recalculated to either only discharge through the sides of the structure or apply the appropriate factor of safety.	Objection: The infiltration rate has been assumed as the 'best case scenario'. The worst-case scenario rate should be used.
		☑ Infiltration drainage storage has half drain down time greater than 24 hours and an alternative design or mitigation is required.	Objection: The infiltration rate has been assumed as the 'best case scenario'. The worst-case scenario rate should be used.
		☑ The post development 100% AEP (or 1 in 1 year) rainfall event runoff rate should also be controlled to the equivalent pre-development rate.	Objection: Pre and Post development surface water runoff rates are in Appendix I which has not been provided. We cannot provide comment until this has been provided.
		Proposed discharge rates and volumes are greater than greenfield with no justification.	Objection: Pre and Post development surface water runoff rates are in Appendix I which has not been provided. We cannot provide comment until this has been provided.
		Proposed discharge rates include future allowances for climate change and / or urban creep. These must be removed, and all calculations resubmitted.	Not included – Urban Creep is not included.
		□ Require justification and supporting calculations for brownfield % betterment and why this can't be closer to the predevelopment greenfield scenario.	Not required – Greenfield Site.
		Proposed discharged rates would increase flood risk elsewhere and need to be re-assessed.	Objection: Pre and Post development surface water runoff rates are in Appendix I

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertford
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	



Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordshire
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

FULL APPLICATION	Related Policy or Standard	Applicant Action Required	LLFA Specific Comment
Location of SuDS		Layout and/or drainage layout drawings need to show all the drainage features (storage and conveyance), with labels the same as those in the submitted supporting calculations.	Objection: Confirmation of any formal drainage on site is required in a drawing. Currently, it is unclear as to whether formal drainage will be used on site.
		Drawings need to show the detailed design (not preliminary issue).	Informative: Drainage drawings, when submitted will need to be detailed design.
		Drawings of cross sections and long sections of all the network and structures such as ponds, basins and swales need to be supplied.	Objection: Confirmation of any formal drainage on site is required in a drawing. Currently, it is unclear as to whether formal drainage will be used on site.
What is the impact of flood risk on the development?	NPPF Paragraph 182	Updated supporting calculations required to show;	
	SDNSTS S7, S8, S9, S10 and S11 Policy WAT5 Sustainable Drainage	☑ revised modelling calculations to use a CV value of 1.	Objection: Calculations are in Appendix H which has not been provided. We cannot provide comment until this has been provided.
		☑ 50% AEP rainfall event does not surcharge in the drainage network if it is to be adopted by a responsible authority.	Objection: Calculations are in Appendix H which has not been provided. We cannot provide comment until this has been provided.
		☑ 3.33% AEP rainfall event plus climate change does not flood outside the drainage network which is designed to hold water.	Objection: Calculations are in Appendix H which has not been provided. We cannot provide comment until this has been provided.

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordsh
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordshire
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

FULL APPLICATION	Related Policy or Standard	Applicant Action Required	LLFA Specific Comment		
		Exceedance of the design 1% AEP rainfall event plus climate change (or failure of the drainage network) must be shown on a drawing, minimising impacts to people and property. This drawing will include proposed external ground levels, finished floor levels and any designed slopes on impermeable surfaces such as highways or car parks.	Objection: The Exceedance Flow Plan is in Appendix I which has not been provided. We cannot provide comment until this has been provided.		
		☑ ½ drain down times need to be submitted and show that they are within 24 hours (or within 48 hours for features that are lined e.g. lined tanks or lined basins).	Objection: Calculations are in Appendix H which has not been provided. We cannot provide comment until this has been provided.		
		Any drainage network showing storage features with ½ drain down time greater than the 24 hours (or 48 hours for lined structures) must be redesigned to show how it can meet this standard or be increased in size to accommodate a subsequent storm event of 3.33% AEP flood event plus climate change allowance.	Objection: Calculations are in Appendix H which has not been provided. We cannot provide comment until this has been provided.		
		☑ The drainage calculations must be shown to include a surcharged outfall to a watercourse or culverted watercourse or watercourse within a sewer. This surcharge level must be the 1% AEP flood event of the receiving watercourse if known or bank full if not already hydraulically modelled.	Objection: Calculations are in Appendix H which has not been provided. We cannot provide comment until this has been provided. The development could discharge to a watercourse.		
How will the drainage and watercourse features be managed and maintained?	NPPF Paragraph 182 PPG Paragraph 055, 057 and 058 SDNSTS S10, S11, S12, S13 and S14	□ High level assessment of the maintenance of any SuDS features and structures and who will be adopting these features for the lifetime of the development.	Included – Section 10.5.		

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertford
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

Site:	Land To The West Of The A507 Between Cottered And Cromer, Hertfordshire, SG9 9PU	Hertfordshire
LPA Reference:	3/24/2245/FUL	Supported by
Date Assessed:	09 January 2024	

FULL APPLICATION	Related Policy or Standard	Applicant Action Required	LLFA Specific Comment
		A high-level assessment of how water quantity and water quality will be managed during the construction phase is required. Identifying high level assumptions such as need to discharge to a sewer or watercourse with appropriate pollution measures.	Objection: A high-level assessment of water quality during construction is required.
Other		□ Bespoke advice	Not required – Covered in checklist.

Annex B – Culvert Upgrade on Ordinary Watercourse

NOTES: 1. FINAL SPECIFICATION AND INSTALLATION METHOD TO BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE RELEVANT AUTHORITIES. 2. CULVERT TYPE AND SIZING TO BE DEFINED DURING DESIGN OF ON-SITE DRAINAGE SYSTEMS. Produced by: Francesco Ghergo Renewable Energy Systems Ltd Registered Office: Beaufort Court, Egg Farm Lane, Kings Langley, Hertfordshire WD4 8LR FG AP RB 2025-01-17 First Issue ISSUE DRAWN CHKD APPD DATE REVISION NOTES PURPOSE COORDINATES PERMITTING N/A SCALE DATUM @A3 N/A 1:75 T-LAYOUT NO LAYOUT DRAWING N/A N/A PROJECT TITLE CUILMORE EXTENSION ----DRAWING TITLE FIGURE 12 INDICATIVE CULVERT WATERCOURSE CROSSING RES DRAWING NUMBER REV 05415-RES-DRN-DR-PT-001 1 THIS DRAWING IS THE PROPERTY OF RENEWABLE ENERGY SYSTEMS LIMITED AND NO REPRODUCTION MAY BE MADE IN WHOLE OR IN PART WITHOUT PERMISSION BEAUFORT COURT, EGG FARM LANE, KINGS LANGLEY, HERTS WD4 8LR. UK TEL +44 (0) 1923 299200 WWW.RES-GROUP.COM

Annex C – Causeway Calculations

	RPS Group I	Plc		File: Invert	ers infiltration	n.pfd	Page 1
CAUSEWAY				Network: S	Storm Networ	k	Cottered Solar
				Caitlin Eva	ns		Inverter Units
				11/04/202	5		
			<u>Design</u>	<u>Settings</u>			
	Rainfall Meth	nodology	FEH-22		Minimum Ve	locity (n	n/s) 1.00
	Return Perio	d (years)	100		Conn	ection T	pe Level Soffits
	Additional	Flow (%)	0	Minin	num Backdrop	Height	(m) 9.000
	Time of Ent	CV	1.000	P	referred Cover	r Depth	(m) 1.000
Maximum Time of	Concentratio	on (mins)	30.00	Enforce	best practice of	design ru	iles √
Maxii	num Rainfall	(mm/hr)	50.0				
			No	<u>des</u>			
				.			
Name	Area (ha)	I Of E (mins)	Level	Diameter (mm)	Easting I	Northing (m)	g Depth (m)
	(114)	((m)	()	()	(,	(,
1		5.00	100.000	1200	1010.000 1	1000.000	0 1.400
2-SOAKAV	VAY 0.007	5.00	100.000	1200	1020.000 1	1000.000) 1.500
			<u>Simulatio</u>	n Settings			
Rainfall Methodology	FEH-22		Analysis	Speed Det	tailed Add	ditional	Storage (m³/ha) 0.0
Summer CV	1.000		Skip Stead	y State x	(Check Di	scharge Rate(s) x
Winter CV	1.000	Drain D	own Time	(mins) 288	80 C	heck Dis	charge Volume x
			Storm D	wrations			
15 60	180	360	600		60 4320	7200	10080
30 120	240	480	720 1	440 288	30 5760	8640)
		<u>.</u>					
K	(vears)	Climate	e Change		Area Additio	onal Flov C %)	N
	100	(0)	40	(470)	0	۹ /۵	0
	<u>Node</u>	2-SOAK/	AWAY Dept	h/Area Stor	age Structure		
Base Inf Coefficient	(m/hr) 0.0	0001	Safety Fac	tor 20		Invert le	evel (m) 98 500
Side Inf Coefficient	(m/hr) 0.0	0001	Poro	sity 1.00	Time to ha	alf empty	/ (mins) 7313304
	Depth	Area	Inf Area	Depth	Area Inf A	rea	
	(m)	(m²)	(m²)	(m)	(m²) (m²	[•])	
	0.000	505.0	505.0	1.500 1	1109.0 110	9.0	

Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	n Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summe	er 1	1	98.600	0.000	0.0	0.0000	0.0000	ОК
960 minute winte	er 2-SOAKAW	/AY 915	98.514	0.014	0.3	7.9089	0.0000	ОК
Link Event (Upstream Depth)	US Node	Link	DS Nod	e	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)
15 minute summer	1 2-SOAKAWAY	1.001 Infiltration	2-SOAKA	AWAY	0.0	0.000	0.000	0.0008

	RPS Group I	Plc		File: spares	s containers.	pfd	Page 1
				Network: S	Storm Netwo	ork	Cottered Solar
CAUSEVVAI				Caitlin Eva	ns		Spares Containers
				11/04/202	5		
			<u>Design</u>	<u>Settings</u>			
	Rainfall Meth	nodology	FEH-22		Minimum V	/elocity (n	n/s) 1.00
	Return Perio	d (years)	100		Con	nection T	ype Level Soffits
	Additional	Flow (%)	0	Minin	num Backdro	p Height	(m) 9.000
	Time of Ent	CV rv (mins)	5.00	P Inclu	referred Cov	er Deptn diate Grou	(m) 1.000
Maximum Time of	Concentratio	on (mins)	30.00	Enforce	best practice	design ri	ules √
Maxir	num Rainfall	(mm/hr)	50.0				
			<u>No</u>	<u>des</u>			
Nomo	A	Toff	Cover	Diamatar	Fasting	Nouthin	a Douth
Name	(ha)	(mins)	Level	(mm)	(m)	(m)	(m)
	()	()	(m)	()	(,	(,	()
1		5.00	100.000	1200	1010.000	1000.00	0 1.400
2-SOAKAV	/AY 0.003	5.00	100.000	1200	1020.000	1000.00	0 1.500
			<u>Simulatio</u>	<u>n Settings</u>			
Rainfall Methodology	FEH-22		Analysis	Speed Det	tailed A	dditional	Storage (m³⁄ha) 0.0
Summer CV	1.000	:	Skip Steady	/ State x		Check Di	scharge Rate(s) x
Winter CV	1.000	Drain D	own Time	(mins) 288	80	Check Dis	scharge Volume x
			Starm D	wations			
15 60	180	360	600 c		50 4320	720	10080
30 120	240	480	720 1	440 288	30 5760	864	0
		1	I	I	I	1	
R	eturn Period	Climate	Change	Additional	Area Addit	tional Flo	w
	(years)	(CC	2%)	(A %)		(Q %)	<u>_</u>
	100		40		0		0
	Node	2-SOAKA	WAY Dept	h/Area Stor	age Structur	<u>e</u>	
Base Inf Coefficient	(m/hr) 0.0	0001	Safety Fac	tor 2.0		Invert L	evel (m) 98.500
Side Inf Coefficient	(m/hr) 0.0	0001	Poros	sity 1.00	Time to h	half empt	y (mins) 7313304
			• •			_	
	Depth (m)	Area I	nf Area	Depth (m)	Area Inf	Area	
	0.000	565.0	565.0	1 500 1	(m) (m) 1690 11	69 0	
	0.000	505.0	505.0	1.500 1	10010 11	00.0	

Page 2 Cottered Solar Spares Containers

Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 100.00%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	i Inflow (I/s)	Node Vol (m³)	Flood (m³)	Status
15 minute summ	ner 1	1	98.600	0.000	0.0	0.0000	0.0000	ОК
360 minute wint	er 2-SOAKAW	VAY 344	98.505	0.005	0.3	2.9263	0.0000	ОК
Link Event (Upstream Depth)	US Node	Link	DS Nod	e	Outflow (I/s)	Velocity (m/s)	Flow/Cap	Link Vol (m³)
15 minute summer	1	1.001	2-SOAK	AWAY	0.0	0.000	0.000	0.0003
360 minute winter	2-SOAKAWAY	Infiltration			0.0			

	RPS Group Pl	lc	File: Comp	ound Infiltration Ter	Page 1
			Network: S	Storm Network	Cottered Solar
CAUSEVVAI U			Caitlin Evar	ns	Substation
			11/04/202	5	
		<u>Design</u>	<u>Settings</u>		
	Rainfall Metho	odology FEH-22		Minimum Velocity (r	n/s) 1.00
	Return Period	l (years) 100	Minim	Connection T	ype Level Soffits
	Auditional F	CV 1 000	Di	referred Cover Denth	(m) 1.000
	Time of Entry	y (mins) 5.00	Inclu	ude Intermediate Gro	und \checkmark
Maximum Time of	Concentration	n (mins) 30.00	Enforce b	best practice design r	ules 🗸
Maxir	num Rainfall (I	mm/hr) 50.0			
		No	odes		
Name	Area (ha)	T of E Cover (mins) Level (m)	Diameter (mm)	Easting Northin (m) (m)	g Depth (m)
1		5.00 100.000	1200	1010.000 1000.00	0 1.400
2-SOAKAV	VAY 0.276	5.00 100.000	1200	1020.000 1000.00	0 1.500
		Simulatio	on Settings		
Rainfall Methodology Summer CV Winter CV	FEH-22 1.000 1.000	Analysis Skip Stead Drain Down Time	Speed Det y State x (mins) 288	cailed Additional Check D 30 Check Di	Storage (m³/ha) 0.0 ischarge Rate(s) x scharge Volume x
15 60 30 120	180 3 240 4	Storm E 360 600 9 480 720 1	Durations 960 216 440 288	50 4320 720 30 5760 864	0 10080 0
R	eturn Period	Climate Change	Additional A	Area Additional Flo	w
	(years)	(CC %)	(A %)	(Q %)	
	100	40		0	0
	Node	2-SOAKAWAY Dep	th/Area Stora	age Structure	
Base Inf Coefficient Side Inf Coefficient	(m/hr) 0.00 (m/hr) 0.00	001 Safety Fac 001 Poro	ctor 2.0 sity 1.00	Invert L Time to half empt	evel (m) 98.500 y (mins) 7313304
	Depth	Area Inf Area	Depth	Area Inf Area	
	(m)	(m²) (m²)	(m)	(m ²) (m ²)	
	0.000 5	565.0 565.0	1.500 1	.169.0 1169.0	

Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 99.98%

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (I/s)	Node Vol (m³)	Flood (m³)	S	tatus
10080 minute summer	1	10140	99.128	0.528	0.0	0.5973	0.0000	SURC	HARGED
10080 minute summer	2-SOAKAWAY	10140	99.128	0.628	2.8	435.0031	0.0000	ОК	
Link Event (Upstream Depth)	US Node	Link		DS Node	Outflo (I/s)	w Velocity (m/s)	y Flow/	Сар	Link Vol (m³)
10080 minute summer	1	1.001	2-S	OAKAWAY	0	.0 0.00	0.	.000	0.3977
10080 minute summer	2-SOAKAWAY	Infiltratio	on		0	.0			

Annex D – Drainage Layout

©) 2024 RPS (Group					
No 1. 2.	otes This drawing appointmen appointmen by its client If received e scale. Only	g has been pro t with its client t. RPS accepts and only for th electronically it written dimens	epared in accor and is subject s no liability for e purposes for is the recipient sions should be	dance with th to the terms a any use of thi which it was p s responsibilit	e scope o ind conditi is docume prepared a ty to print f	f RPS ions of nt oth and pro to corr	s f that er than ovided. ect
3.	This drawing and specific	g should be re ations.	ad in conjuncti	on with all oth	er relevan	t draw	ings
/							
	Gravel S	Sub Base ve Solar P'	KE` V Array				
	Site Bo	undary					
1 \	Conceptual Description	Drainage Stra	ategy		TH By	FC Ckd	10:04:25 Date
	Client Elgin Energy						
	Project	Cottere	d Solar I	⁻ arm			
	Title	Concep Sheet 1	otual Dra I	inage S [:]	trateg	У	
	Status DRAFT Task Team Manager FC Document N HLEF85	^{lumber} 532-RPS	Scale 1:1 @ Information Author FC -P-CDS-D	₽A1 R-1-1004	Date Cru 10.04 Task Inf Manage	eated 1.25 format r	ion
	RPS Project HLEF 855	Number 532 9.com				Rev 1	ision
	. <u></u>						

